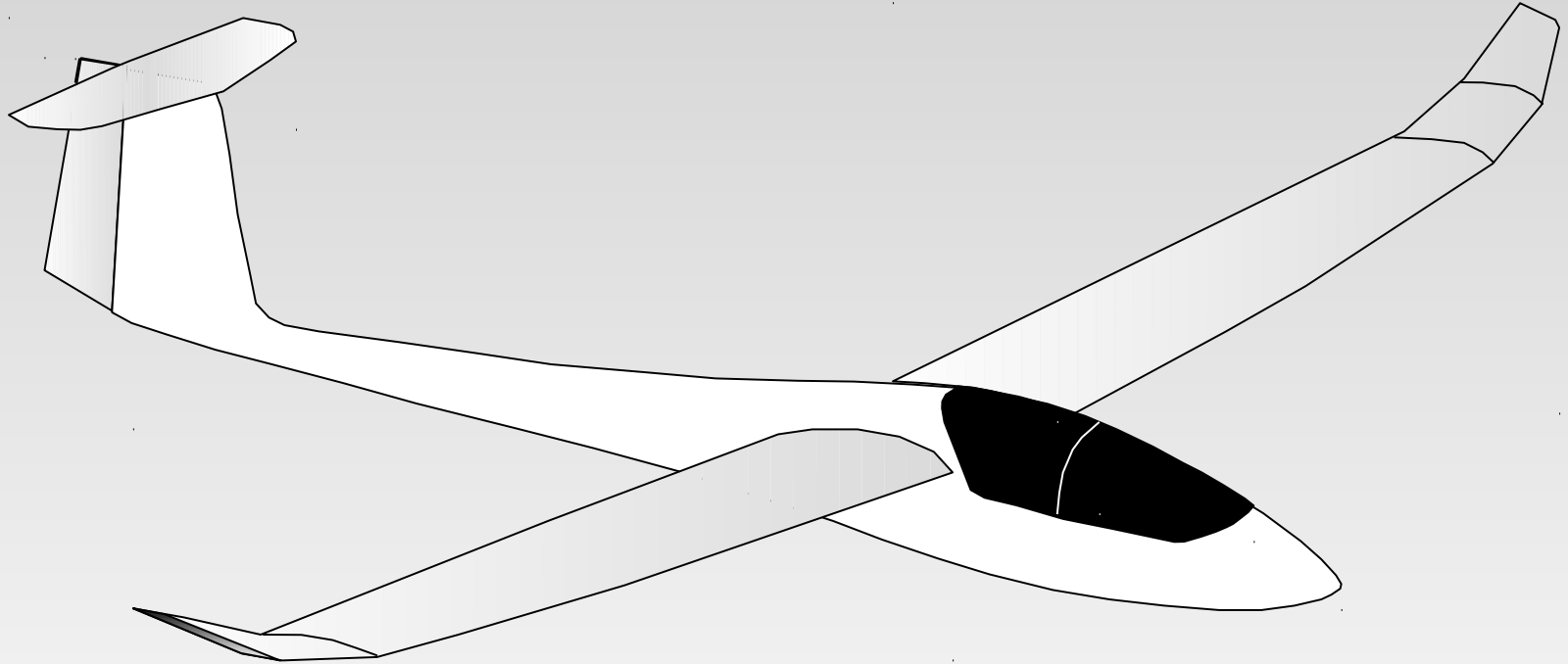


# F.A.Q : Why do I get the message "Point is out of the flight envelope ?"



# About viscosity

- The error message is indirectly a consequence of the fluid's viscosity, so that's a good point to start
- The air in which the plane flies is viscous ; its viscosity is characterized by
  - The dynamic (absolute) viscosity :  $\mu$  [kg/m/s]
  - or by the kinematic viscosity :  $\nu$  [m<sup>2</sup>/s] or [centistokes]
- Both constants are linked by :  $\mu = \rho \cdot \nu$   
where  $\rho$  is the fluid's density [kg/m<sup>3</sup>]

# The Reynolds Number in general

$$Re = \frac{CV}{\nu}$$

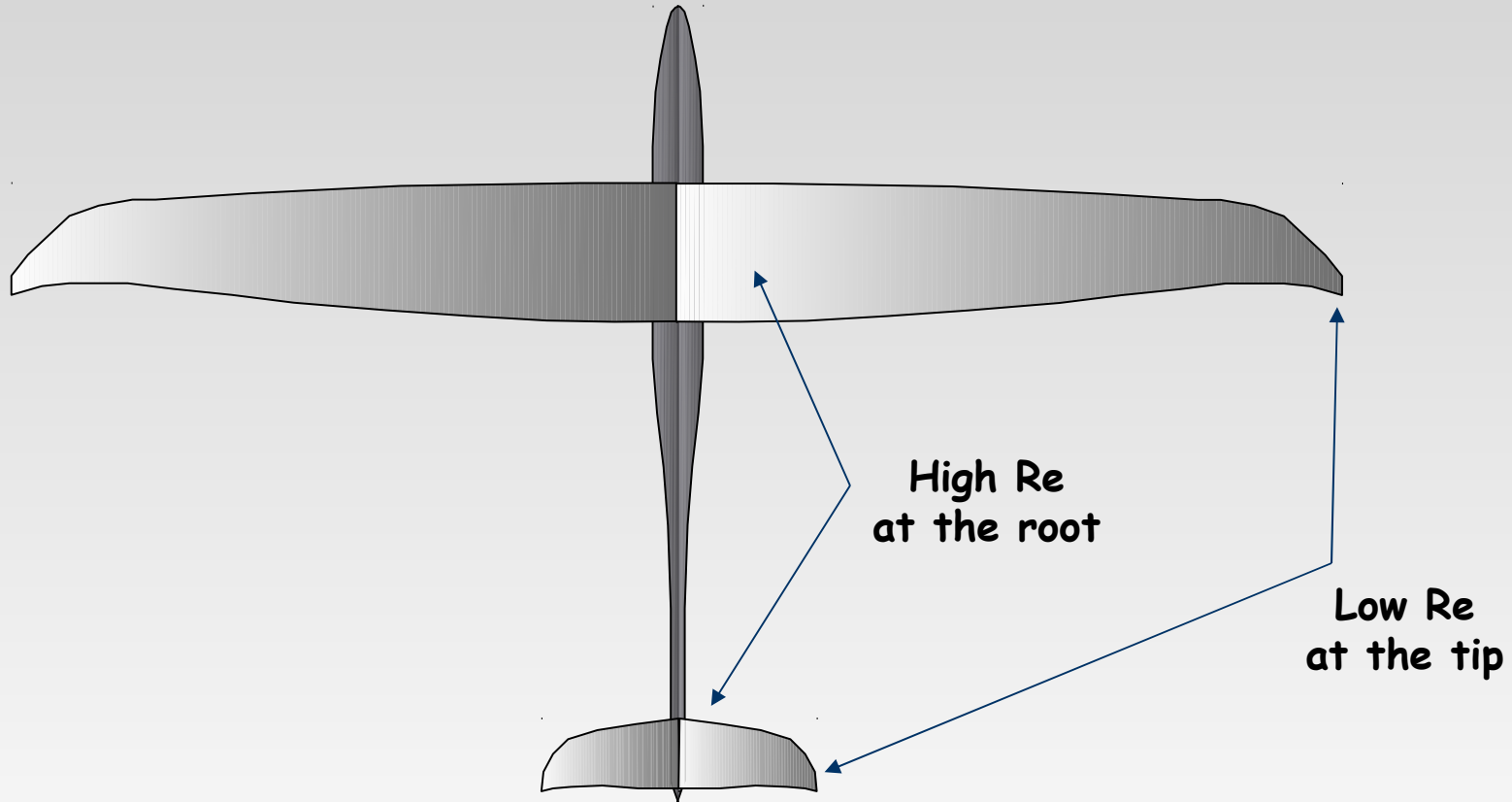
- With  $C$  being a reference length
- $V$  is the fluid's freestream speed
- $\nu$  is the fluid's kinematic viscosity

## The Reynolds Number $Re$ :

- is a dimensionless coefficient
- is a measure of the ratio of inertia forces to viscous forces : the greater the speed, the lower the impact of viscous forces

# The Reynolds model applied to an aircraft

- The usual reference length  $C$  is the local chord
- Hence, the Re Number depends on the span location



# Induced drag and viscous drag

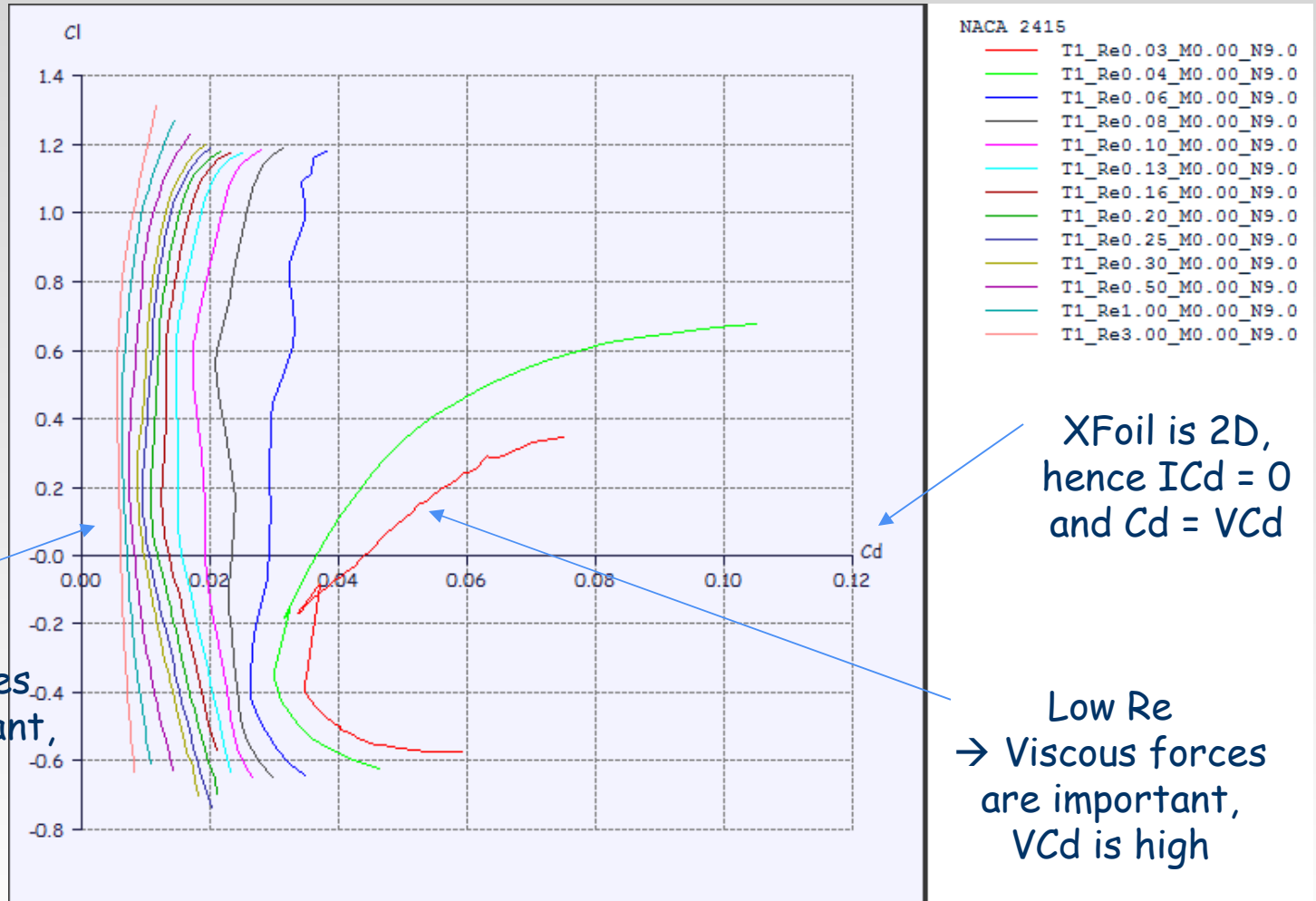
- The induced drag is related to the kinematic energy given by the plane to the fluid, and depends on the plane's speed :  $\text{Induced Drag} = \frac{1}{2} \rho S V^2 ICd$ 
  - $ICd$  does not depend on the plane's speed
- As can be guessed, the viscous drag is a result of the fluid's viscosity :  $\text{Viscous Drag} = \frac{1}{2} \rho S V^2 VCd$ 
  - $VCd$  depends on the plane's speed, and therefore on the Reynolds Number

We illustrate  
this graphically  
in the next slide



# The viscous drag coefficient $VCd$

- It would be easier if  $VCd$  did not depend on  $Re$ , like  $ICd$ , but that is not the case. It can be seen by running a batch analysis with XFOIL



# Viscous and non-viscous behaviour

- The classic (linear) LLT, the VLM, and the 3D panel methods are derived from non-viscous (inviscid) assumptions for the fluid
- Therefore the results from these methods
  - ignore the viscous drag
  - are independent of speed
- Unfortunately, for the size and speed of our model aircraft, **the viscous drag cannot be ignored**
- Since there is no adequate theory to take into account viscosity in 3D analysis for the Re numbers of our model aircraft, we extrapolate it from 2D

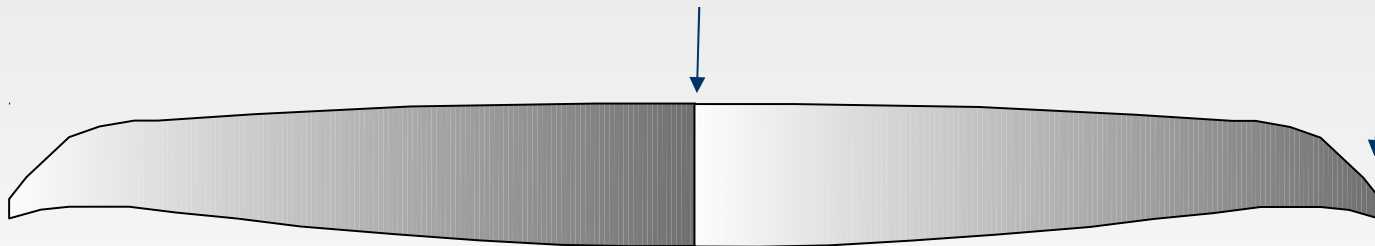
**Not really satisfactory,  
but is the best we can do ☹**

# An example

Consider a wing with span	1 500 mm
The airplane flies at	15 m/s
The root chord is 200 mm =	0.20 m
The tip chord is 30 mm =	0.03 m
The air's kinematic viscosity is $\nu$ =	$1.5 \cdot 10^{-5} \text{ m}^2/\text{s}$
The foil is the NACA 2412 for the whole span	

$$\begin{aligned} Re_{\text{Root}} &= 0.2 \times 15 / 1.5 \cdot 10^{-5} \\ &= 200,000 \end{aligned}$$

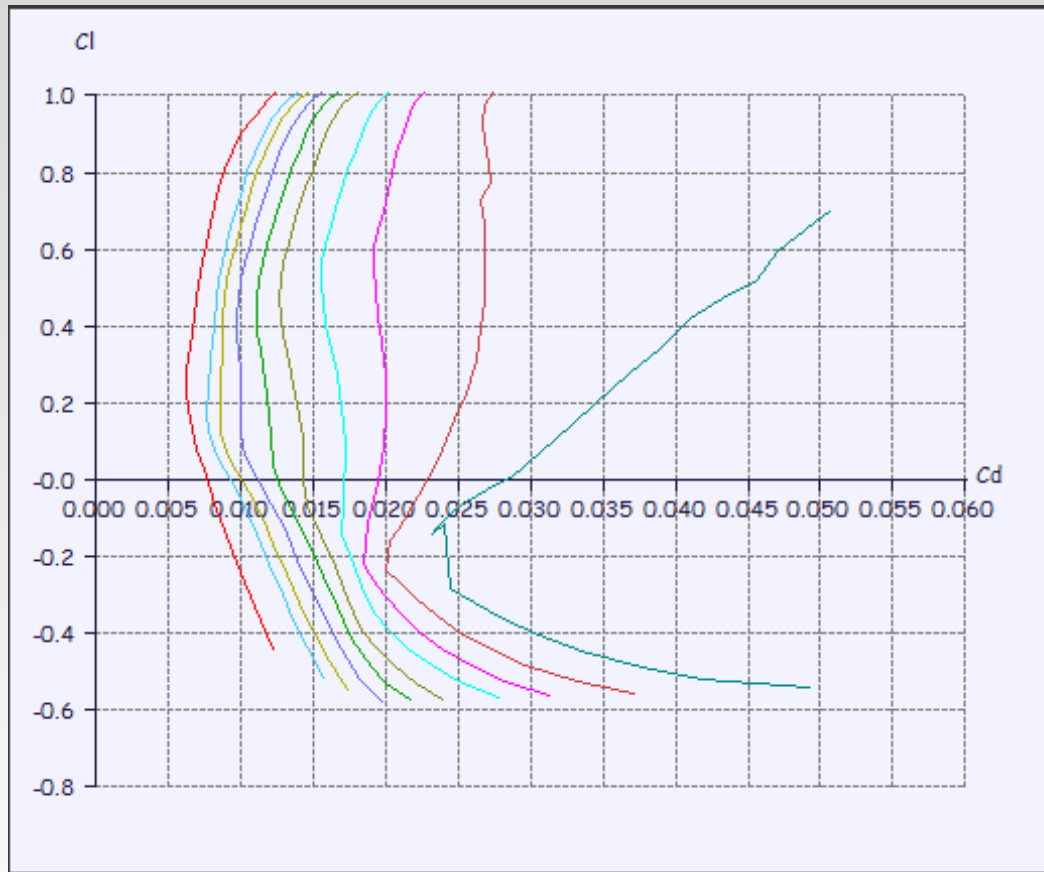
$$\begin{aligned} Re_{\text{Tip}} &= 0.03 \times 15 / 1.5 \cdot 10^{-5} \\ &= 30,000 \end{aligned}$$





# First we generate the viscous polars for the foil

This is done in the "Application/XFoil Direct Analysis" menu, using the "Polars/Run Batch Analysis command"



NACA 2412

- T1\_Re0.04\_M0.00\_N9.0
- T1\_Re0.06\_M0.00\_N9.0
- T1\_Re0.08\_M0.00\_N9.0
- T1\_Re0.10\_M0.00\_N9.0
- T1\_Re0.13\_M0.00\_N9.0
- T1\_Re0.16\_M0.00\_N9.0
- T1\_Re0.20\_M0.00\_N9.0
- T1\_Re0.25\_M0.00\_N9.0
- T1\_Re0.30\_M0.00\_N9.0
- T1\_Re0.50\_M0.00\_N9.0

Our foil  
polar mesh  
runs from  
 $Re=40\ 000$   
to  
 $Re=500\ 000$

# Next we analyze the wing

**Polar Analysis**

Test Wing  
 Auto Analysis Name T1-15.0 m/s-VLM2- 0.00mm

Polar Type  
 Type 1 (Fixed Speed)  Type 2 (Fixed Lift)  Type 4 (Fixed Alpha)

Airplane and Flight Data  
Free Stream Speed 15.00 m/s  
Plane Weight 500.000 g  
Angle of Attack 0.00 °  
Mom. ref. location 0.00 mm

Flight Characteristics  
Wing Loading 23.072 g/dm<sup>2</sup>  
Root Re = 200 000  
Tip Re = 30 000

Solution method  
 LLT  
 VLM  Classic  
 Quads  
 3D Panels

Aerodynamic Data  
Unit  International  Imperial  
ρ = 1.226 kg/m<sup>3</sup>  
ν = 1.500e-5 m<sup>2</sup>/s

Options  
 Viscous Wake...  
 Tilt Geometry  Wake Roll-Up  
 Plane's wings as thin surfaces

Ground effect  
 Ground Effect  
Height = 0.00 mm

OK Cancel

← We generate a polar analysis

And we launch the analysis for  $\alpha=1^\circ$  →

# Results

- Unfortunately, nothing is generated : why ?
- The error messages showed up too fast to read during the analysis, so we call the XFLR5.log file from the "Operating Point" menu

Note : the ".log" file extension is usually associated by default to the notepad, check the association if nothing shows up

```
Test Wing
July 25, 2008 at 20:27:04
```

---

```
Solving the problem...
```

```
Creating the influence matrix...
Solving the linear system...
Calculating the vortices circulations...
```


```
...Alpha=1.00
Calculating induced angles...
Calculating aerodynamic coefficients...
Calculating wing...
```

```
Span pos = -679.00 mm, Re = 36 786, Cl = 0.25 is outside the flight envelope
Span pos = 679.00 mm, Re = 36 786, Cl = 0.25 is outside the flight envelope
```


The interpolation fails



We have a problem at the tip



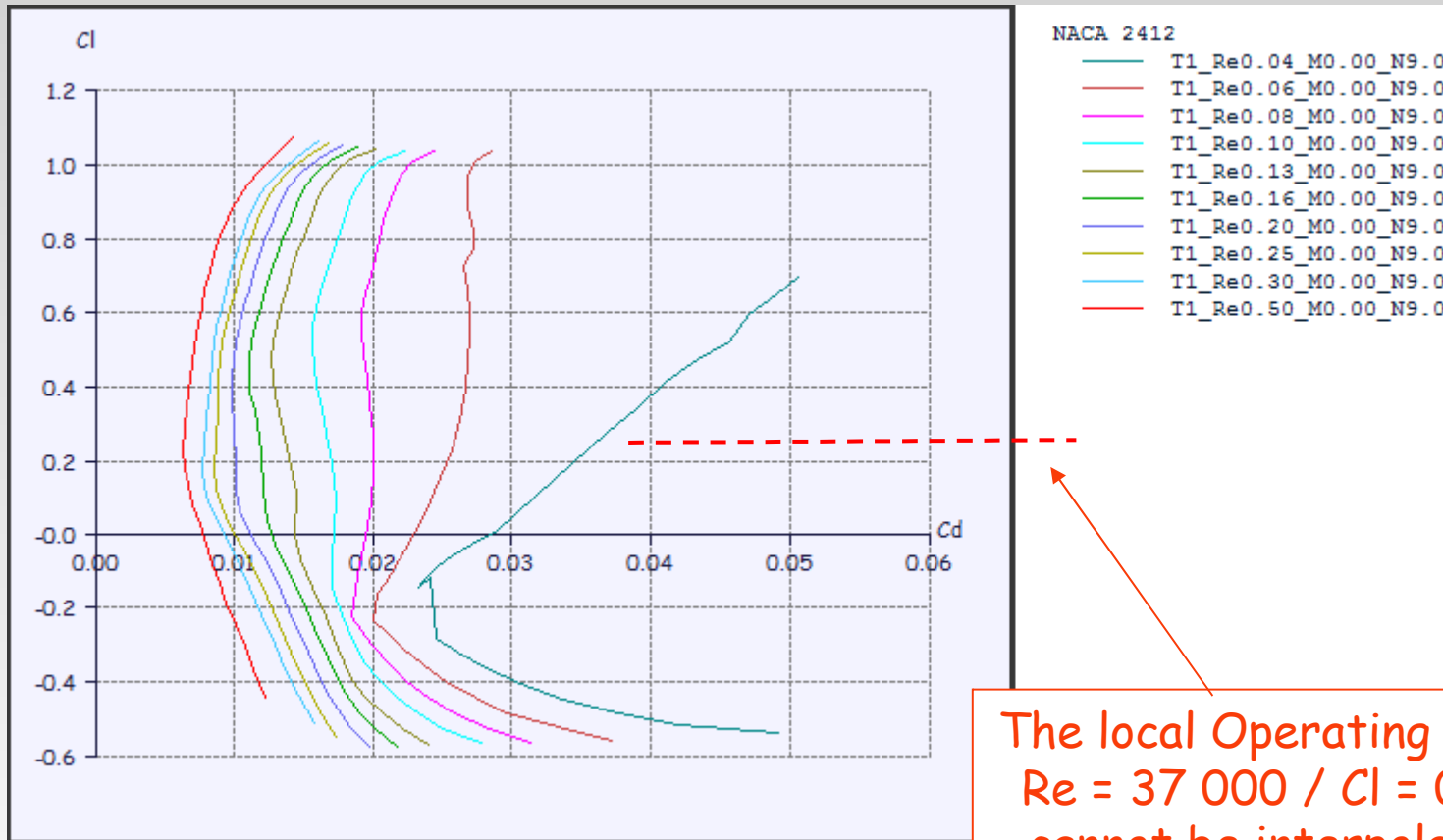
The calculated Re at 15 m/s is less than the min value of the polar mesh, which is 40 000



We illustrate this graphically in the next slide



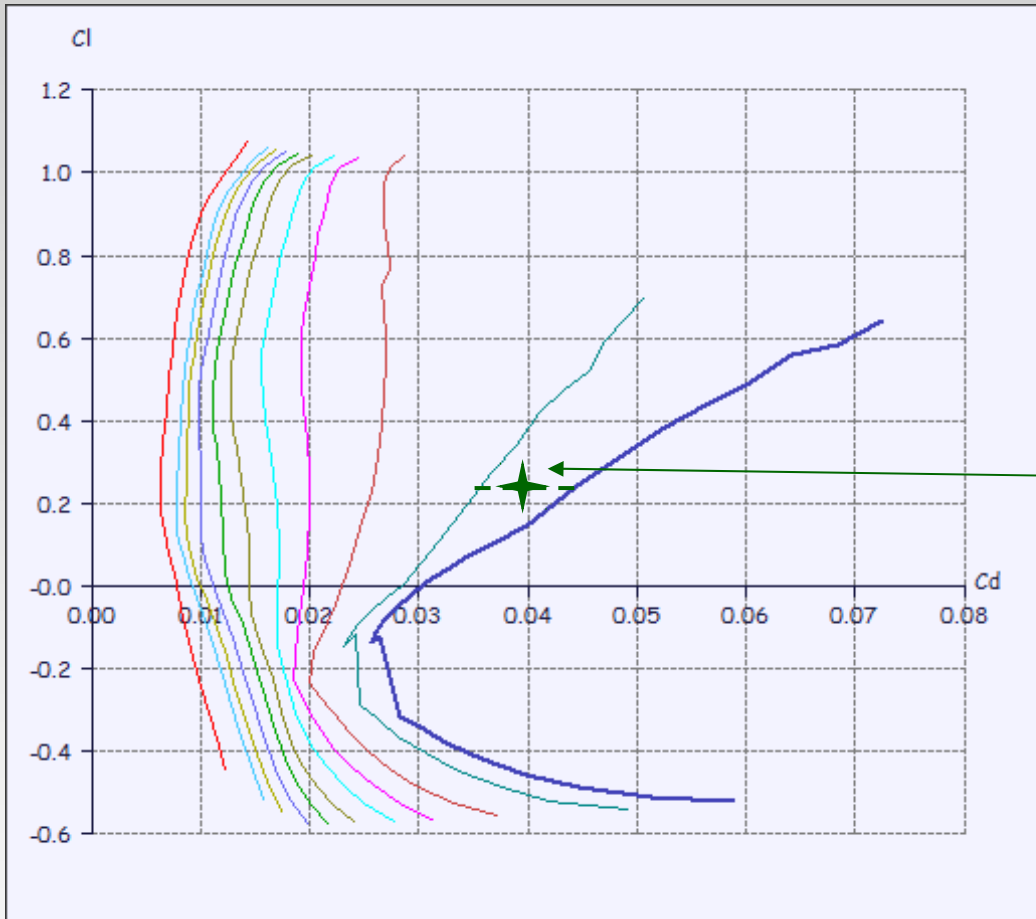
# Interpolating from 2D results at tip chord



# The Fix

We extend the polar mesh down to

$Re_{\xi} = 30\ 000$



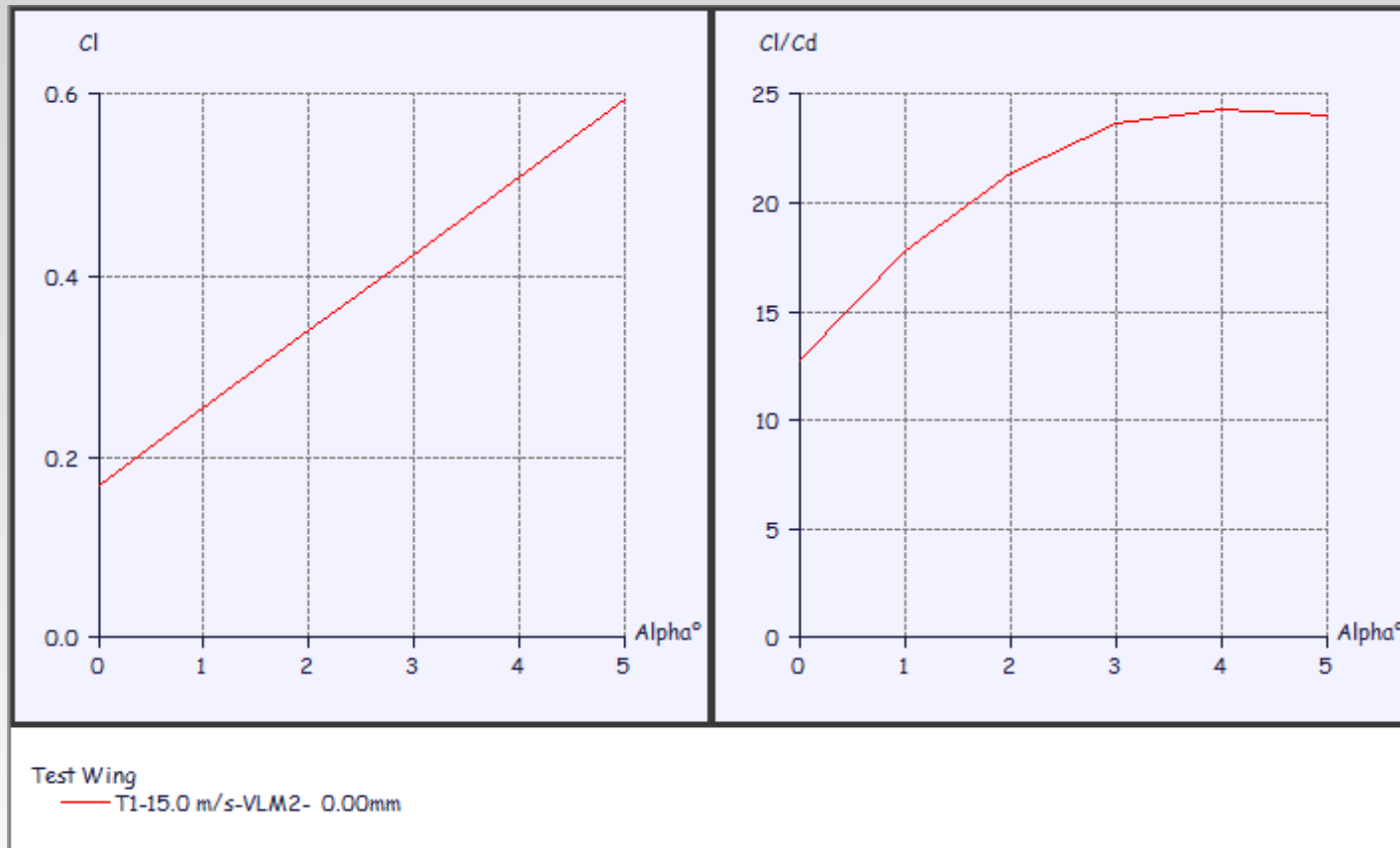
The local Operating point  
 $Re = 37\ 000 / Cl = 0.25$   
can now be interpolated

No more issue for  $\alpha = 1^\circ$

... so we boldly run an analysis from  $\alpha = 0^\circ$  to  $\alpha = 10^\circ$

# Wing Analysis Results from $\alpha = 0^\circ$ to $\alpha = 10^\circ$

Unfortunately, the analysis does not run higher than  $\alpha = 5^\circ$  : why ?



We check again the log file



# Using the log file information

Test Wing  
July 25, 2008 at 20:45:17

---

Solving the problem...

```
Creating the influence matrix...
Solving the linear system...
Calculating the vortices circulations...
...Alpha=0.00
  Calculating induced angles...
  Calculating aerodynamic coefficients...
  Calculating wing...
```

[...]

```
...Alpha=6.00
  Calculating induced angles...
  Calculating aerodynamic coefficients...
  Calculating wing...
```

```
Span pos = -679.00 mm, Re = 36 786, Cl = 0.65 could not be interpolated
Span pos = 679.00 mm, Re = 36 786, Cl = 0.65 could not be interpolated
```

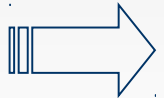
The problem is  
still at the tip

The Re is OK

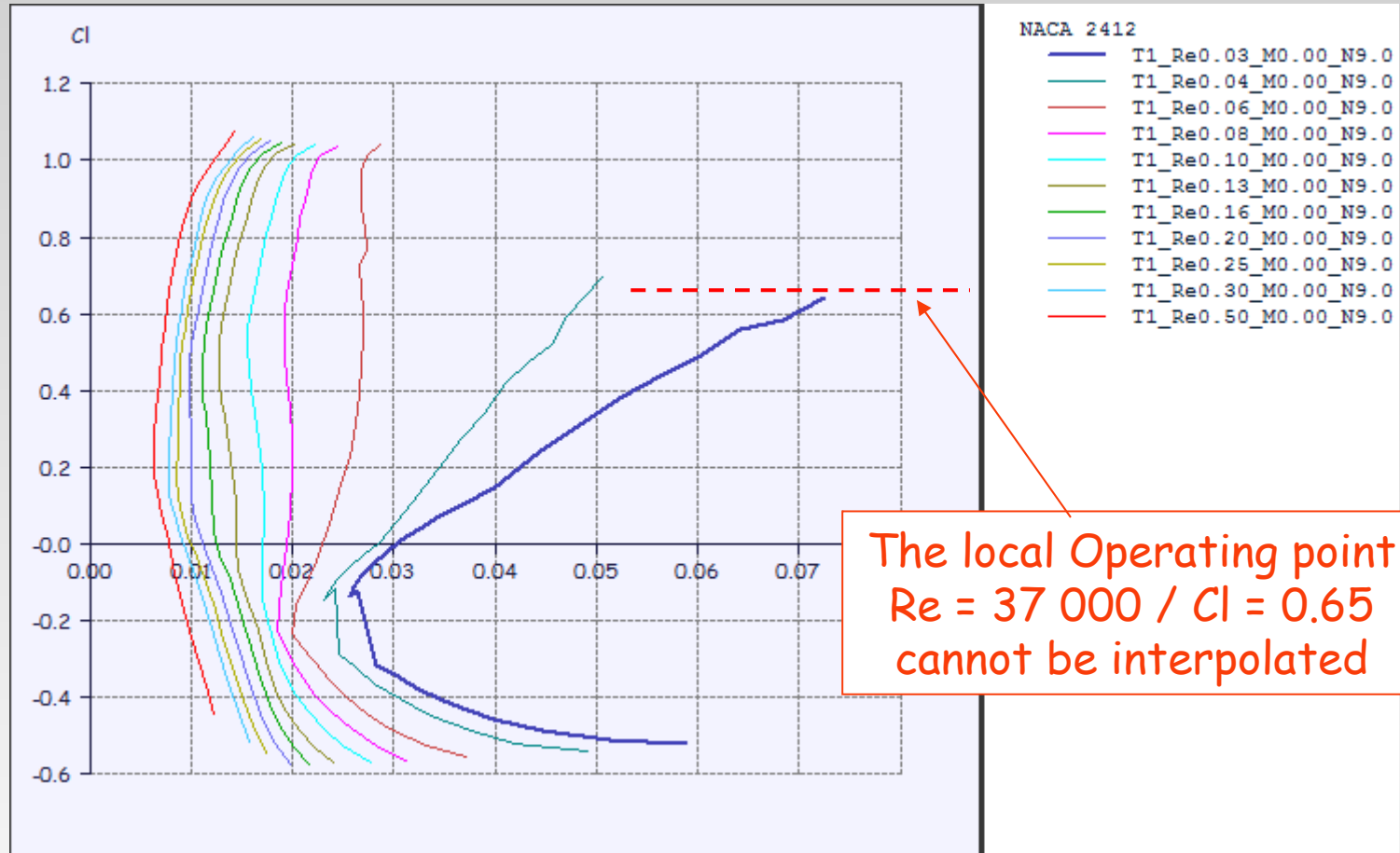
Unfortunately the foil's Type 1 polar  
mesh does not extend to  $Cl=0.65$  for  
 $Re=30\ 000$  : the interpolation fails



We illustrate  
this graphically  
in the next slide



# Interpolating from 2D results at high incidence





# The fix

- We try to extend the foil polar mesh at high a.o.a for  $Re = 30\ 000$  to achieve  $Cl$  values higher than 0.65
  
- Two possibilities :
  1. The XFoil analysis converges for  $Re = 30k$  and  $Cl > 0.65$   
→ we have fixed the issue and may run the wing analysis with success
  2. The XFoil analysis does not converge  
→ we have reached the limits of the 2D approximation for the viscous drag ;

**In fact, the approximation is most probably quite questionable long before this point is reached**

**In the hope that  
this helped !**

